

# On the catalytic effect of Pd(s) on the reduction of $\text{UO}_2^{2+}$ with $\text{H}_2$ in aqueous solution

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## Abstract

The catalytic effect of Pd(s) (as a model for noble metal particles) on the reduction of  $\text{UO}_2^{2+}$  by  $\text{H}_2$  has been studied experimentally. The experiments were performed in aqueous solution in an autoclave. The aqueous solutions were pressurized with  $\text{H}_2$  or  $\text{N}_2$  and the  $\text{UO}_2^{2+}$  concentration was measured as a function of time. The experiments clearly show that Pd catalyzes the reaction between  $\text{UO}_2^{2+}$  and  $\text{H}_2$ . The rate constant of the reaction was found to be close to diffusion controlled and independent of the  $\text{H}_2$  pressure in the range 1.5–40 bar. The effect of a catalyzed reduction of U(VI) to U(IV) in the solid phase is also discussed.

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## 1. Introduction

In Sweden, the radioactive spent nuclear fuel will be placed in a deep repository according to the KBS-3 model, developed by The Swedish Nuclear Fuel and Waste Management Co, SKB. The fuel will be encapsulated in canisters made of copper with an insert of steel, surrounded by bentonite clay and placed 500 m under the ground. One of the key questions for the safety assessment of the spent nuclear fuel repository is the rate of radiation induced dissolution of the fuel matrix,  $\text{UO}_2$ , followed by the subsequent release of actinides and fission products. In the event of canister failure, the highly radioactive spent nuclear fuel will cause radiolysis of the groundwater. Radiolysis of groundwater will produce both oxidants ( $\text{OH}^\cdot$ ,  $\text{H}_2\text{O}_2$ ,  $\text{HO}_2^\cdot$  and  $\text{O}_2$ ) and reductants ( $e_{\text{aq}}^-$ ,  $\text{H}^\cdot$  and  $\text{H}_2$ ). For kinetic reasons, the oxidants will react with  $\text{UO}_2$  producing soluble U(VI). The most important oxidant under deep repository conditions has been shown to be  $\text{H}_2\text{O}_2$  [1]. As  $\text{H}_2\text{O}_2$  is both radiolytically produced and consumed by reduction at the fuel surface, the concentration of  $\text{H}_2\text{O}_2$

will eventually approach a steady state. The time to approach the surface steady state concentration is sufficiently short to be neglected compared to the times of interest when considering a deep repository [2].

$\text{HCO}_3^-$  present in the groundwater increases the otherwise slow dissolution of the fuel matrix due to formation of water soluble complexes with  $\text{UO}_2^{2+}$  formed upon oxidation of  $\text{UO}_2$  [3]. Swedish groundwater contains  $\sim 2$  mM carbonate [4]. The effect of  $\text{HCO}_3^-$  on  $\text{H}_2\text{O}_2$  induced oxidative dissolution of  $\text{UO}_2$  is a linear increase of the rate as a function of  $[\text{HCO}_3^-]$  from 0 to 1 mM. Above 1 mM the rate is independent of the  $\text{HCO}_3^-$  concentration and the reaction is limited by oxidation [5]. Under these conditions, the surface area available for oxidation can be considered constant with time.

Due to anaerobic corrosion of the iron in the canister large amounts of  $\text{H}_2$  are expected to be produced in case of canister failure [6].  $\text{H}_2$  is also produced in the radiolysis of water. Experiments on spent fuel, MOX and  $\alpha$ -doped  $\text{UO}_2$  show that the dissolution rate is lower than expected from the amount of  $\text{H}_2\text{O}_2$  produced radiolytically. These experiments were performed at various hydrogen pressures and indicate that the oxidative dissolution rate is reduced in the presence of dissolved hydrogen, but the mechanism is still largely unknown [7].  $\text{H}_2$  slowly reduces U(VI) to

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U(IV) and it also reacts with the radiolytically produced oxidants [8]. However, these effects are of marginal importance and cannot explain the dramatic reduction in dissolution rate.

Some of the fission products in the spent fuel form nanometer sized noble metal particles, often referred to as  $\epsilon$ -phase or  $\epsilon$ -particles, containing Mo, Ru, Tc, Pd and Rh [9]. The content of noble metal particles in spent nuclear fuel is estimated to be  $\sim 1\%$  [10]. From previous experiments these particles are known to catalyze reductions by  $H_2$  [11]. In a recent study we showed that Pd catalyzes the reduction of  $H_2O_2$  by  $H_2$ . Even though the catalysis is very efficient, this reaction would only have a small effect on the dissolution rate. One percent surface coverage of Pd would reduce the rate by a factor 3.9 [12].

It is also possible that Pd catalyzes the otherwise slow reduction of U(VI) to U(IV) by  $H_2$ . This will not affect the dissolution rate, but it will lower the concentrations of redox sensitive radionuclides in the aqueous phase. The reduction of  $UO_2^{2+}$  by  $H_2$  has been studied before and the activation energy for the reaction has been found to be 130 kJ/mol [8]. The reaction was also studied in the 1950s using nickel as a catalyst resulting in an activation energy of 41 kJ/mol [13]. Cobalt and platinum were also shown to catalyze the reaction. Even  $UO_2$  has been suggested to catalyze the reaction, but recent experiments have not supported this theory [8].

In this work we have studied the possible catalytic effect of Pd (as a model for noble metal particles) on the reduction of  $UO_2^{2+}$  by  $H_2$  at room temperature.

## 2. Experimental

All experiments were performed in a glass vessel placed inside an autoclave. The autoclave is equipped with inlet and outlet tubes for pressurizing and sampling and also a stirrer. The Pd powder and 280 ml 2 mM  $NaHCO_3$  was bubbled with  $N_2$  for 20 min. The mixture was put in the autoclave and  $N_2$  was blown through for 10 min. The autoclave was then pressurized with  $H_2$  and left overnight with continuous stirring. The amount of Pd powder was varied between 0 and 35 mg. The following day, 20 ml  $1.5 \times 10^{-4}$  M  $UO_2(NO_3)_2 \cdot 6H_2O$  solution was added to give a final concentration of  $1 \times 10^{-5}$  M. The concentration of  $UO_2^{2+}$  was measured as a function of reaction time for at least 90 min using UV/visible spectroscopy. The concentration was measured with the reagent Arsenazo III (1,8-dihydroxynaphthalene-3,6-disulphonic acid-2,7-bis[(azo-2)-phenylarsonic acid]). Arsenazo III forms colored 1:1 complex with a number of 2+ and 3+ charged cations, for example  $UO_2^{2+}$ . The  $UO_2^{2+}$ -Arsenazo III complex absorbs at 653 nm. The sample volume taken for analysis was approximately 3 ml to enable doublet samples. Detailed information about the Arsenazo III method can be found in Refs. [14,15].

In order to study if the possible catalytic effect was dependent on the  $H_2$  pressure, experiments were performed with 33 mg Pd varying the  $H_2$  pressure between 1.5 and

40 bar. Experiments without  $H_2$  were also performed. Chemicals and gases came from Merck, AGA and Air Liquid. Milli-Q filtered water was used throughout and all experiments were performed at room temperature.

## 3. Results and discussion

In the experiments with  $UO_2^{2+}$ , Pd and  $H_2$ , the concentration of  $UO_2^{2+}$  was decreasing with reaction time indicating a catalytic effect of Pd. This is illustrated in Fig. 1. The concentration of  $UO_2^{2+}$  did not change with time in the absence of Pd or  $H_2$ . The rate of the reaction is increasing with the amount of Pd.

By plotting  $\ln([A]/[A]_0)$  against the reaction time we obtain the pseudo-first-order rate constants,  $k_1$  ( $s^{-1}$ ) from the slopes. The resulting pseudo-first-order rate constants are given in Table 1. By plotting  $k_1$  ( $s^{-1}$ ) against the solid surface/total solution volume,  $S/V$  ( $m^{-1}$ ) the second order rate constant,  $k$  ( $m s^{-1}$ ), is determined from the slope. This is shown in Fig. 2. The second order rate constant is  $(1.5 \pm 0.1) \times 10^{-5} m s^{-1}$ , which corresponds to the diffusion limit of the system and an activation energy close to zero. The activation energy does not differ significantly from the Pd catalyzed reaction between  $H_2O_2$  and  $H_2$ , for which the rate constant was found to be  $(2.1 \pm 0.1) \times 10^{-5} m s^{-1}$  [12]. The solid surface area was calculated using the average particle radius (0.625  $\mu m$ ) assuming spherical geometry.

When varying the  $H_2$  pressure between 1.5 and 40 bar at room temperature we could not observe any increase in the

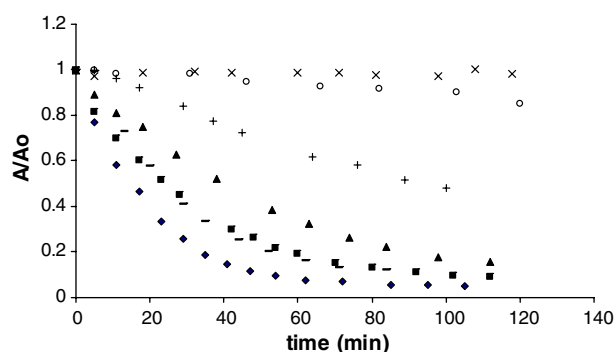


Fig. 1. Normalized concentration of  $UO_2^{2+}$  plotted against reaction time at 40 bar  $H_2$  with different amounts of Pd (+ 4 mg, ▲ 8 mg, ■ 16 mg, ◆ 24 mg, ◆ 35 mg, × 32 mg Pd without  $H_2$  ( $N_2$  instead), ○ without Pd).

Table 1  
Pseudo-first-order rate constants for different amounts of Pd ( $S/V$  ratios) at 40 bar  $H_2$

Pd (mg)	$S/V$ ( $m^{-1}$ )	$k_1$ ( $s^{-1}$ )
4	5.33	$1.35 \times 10^{-4}$
8	10.67	$2.79 \times 10^{-4}$
16	21.33	$4.52 \times 10^{-4}$
24	32	$5.88 \times 10^{-4}$
35	44	$7.83 \times 10^{-4}$

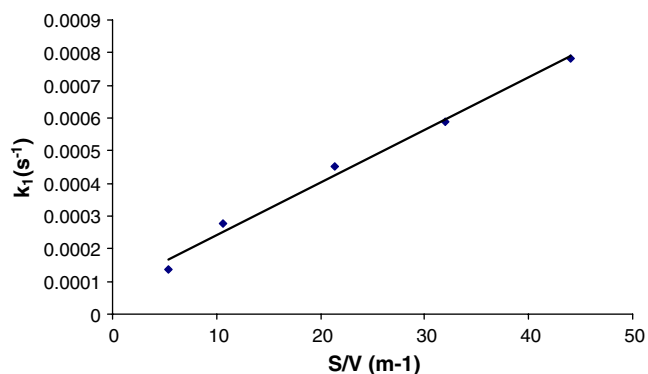


Fig. 2. Pseudo-first-order rate constants,  $k_1$  ( $\text{s}^{-1}$ ), plotted against the solid surface area/total solution volume ratio,  $S/V$  ( $\text{m}^{-1}$ ) at 40 bar  $\text{H}_2$ .

reaction rate. In the previous experiments where nickel was used as a catalyst, the rate of the reaction was found to be directly proportional to the hydrogen pressure [13]. An explanation to why this effect is not seen here could be that Pd can absorb significant amounts of  $\text{H}_2$ , up to 935 times its own volume [16]. Hence, the dynamics of  $\text{H}_2$  absorption does not affect the reaction rate under the present conditions.

As shown above, Pd catalyzes the reduction of U(VI) to U(IV) by  $\text{H}_2$  in solution. For 100 year old fuel and 38 MWd/kg burnup, the maximum dissolution rate is expected to be  $4.94 \times 10^{-10} \text{ mol m}^{-2} \text{ s}^{-1}$  based on a steady state approach for  $\text{H}_2\text{O}_2$  [17]. Under these conditions, the U(VI) steady state concentration in solution (i.e. the concentration at which the rate of dissolution of U(VI) is equal to the rate of U(VI) reduction by  $\text{H}_2$ ) is  $\sim 3 \mu\text{M}$ , assuming a noble metal particle content of 1% and 40 bar  $\text{H}_2$ .

The catalytic effect of noble metal particles studied here is not expected to affect the dissolution of the spent nuclear fuel. But if the same reaction occurs in the solid phase, this would inhibit the dissolution of the fuel much more efficiently. In the solid phase, noble metal particles can catalyze the reduction of undissolved oxidized  $\text{UO}_2$  by  $\text{H}_2$ , thus preventing dissolution of the oxidized  $\text{UO}_2$ . This requires galvanic coupling between the  $\text{UO}_2$  matrix and the noble metal particles. This coupling has been verified in electrochemical studies on SIMFUEL [18]. The noble metal particle catalyzed reduction (which is most likely diffusion controlled [12]) will compete with dissolution of oxidized  $\text{UO}_2$ . The rate of the latter reaction depends on the  $\text{HCO}_3^-$  concentration. This would explain why the dissolution in the presence of  $\text{H}_2$  is slower than expected. By putt-

ing the reduction rate of U(VI) in the solid phase equal to the oxidation rate of U(IV), one can calculate that a noble metal particle content of only 1 ppm on the surface is enough to completely cancel the dissolution (40 bar  $\text{H}_2$ , 100 year old fuel). Previous long term leaching experiments on spent nuclear fuel indicate that the rate of dissolution approaches zero at 0.1 bar  $\text{H}_2$  (produced from radiolysis) [19]. Experiments are now being performed using solid Pd-doped  $\text{UO}_2$  pellets to quantitatively examine the inhibiting effect of  $\text{H}_2$  on oxidative dissolution proposed above.

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